



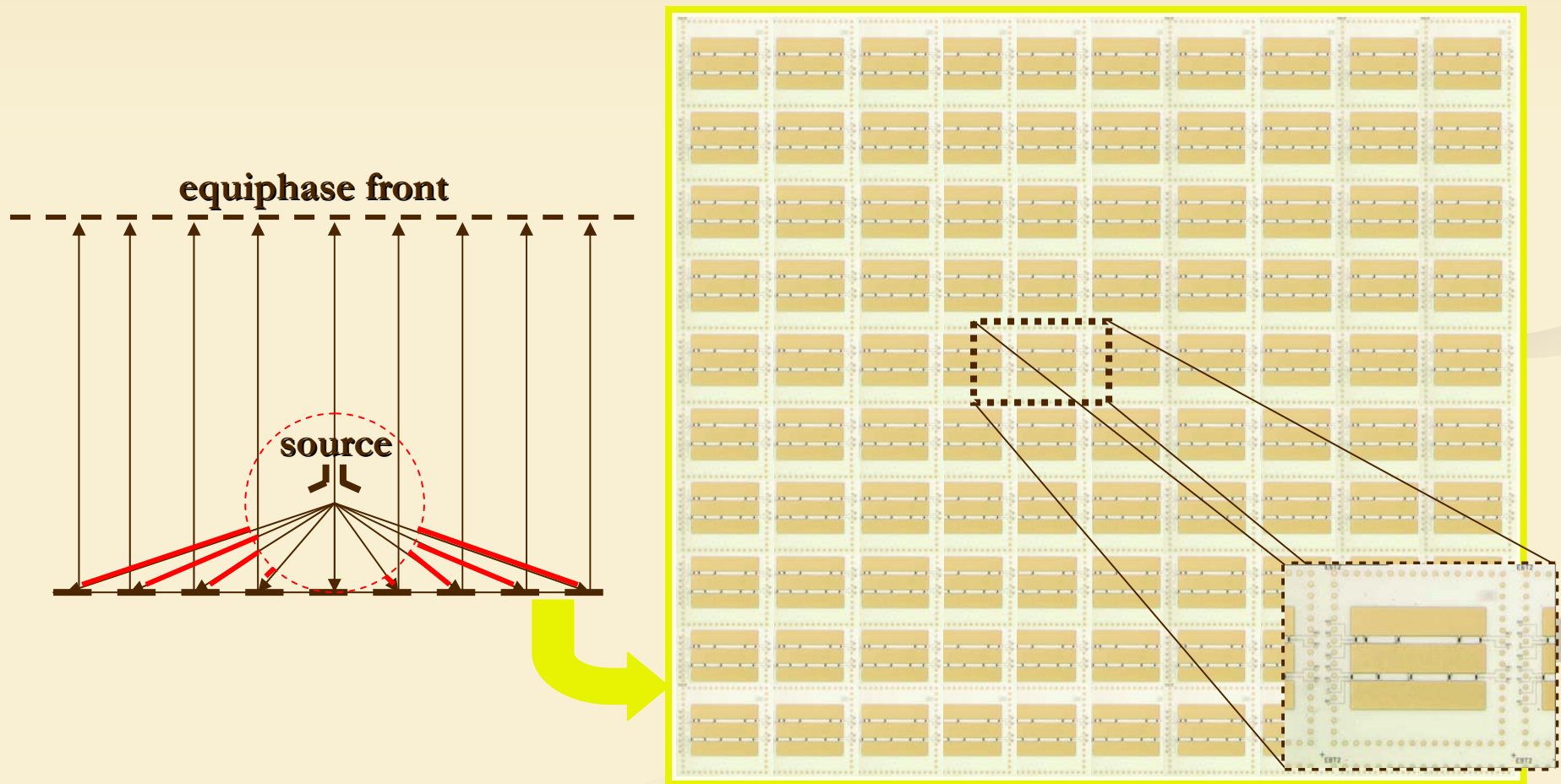
Journées scientifiques du LAAS-CNRS
40ème anniversaire
7, 8 et 9 Octobre 2008

Electromagnetism and Multi-scale Structures

Hervé Aubert

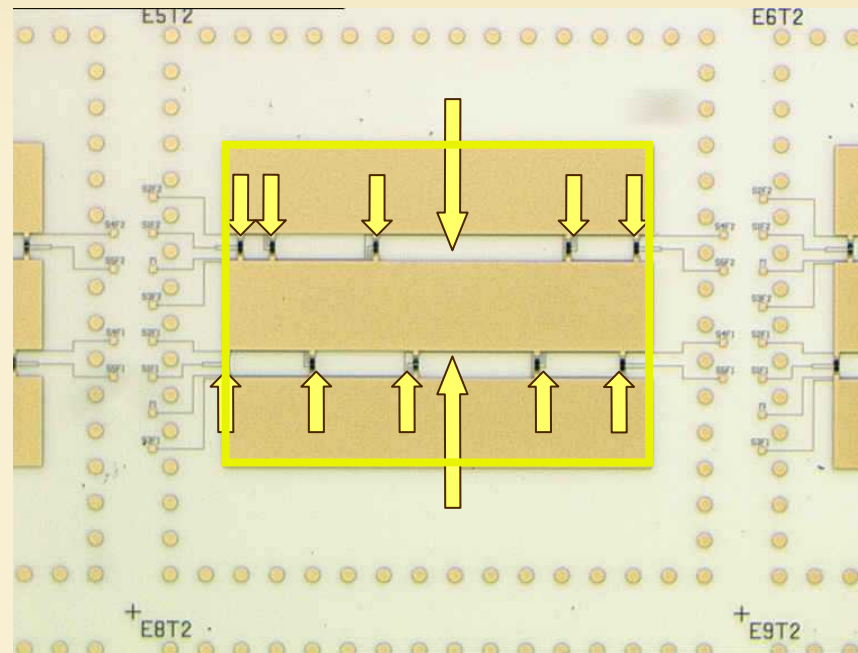
LAAS-CNRS, Toulouse University, France
INPT-ENSEEIH, Toulouse, France

EXAMPLE :
RECONFIGURABLE REFLECTARRAY WITH
NON-IDENTICAL CELLS



MEMS-Controlled Phase shifter Elements for a Linearly Polarised Reflectarray (*)

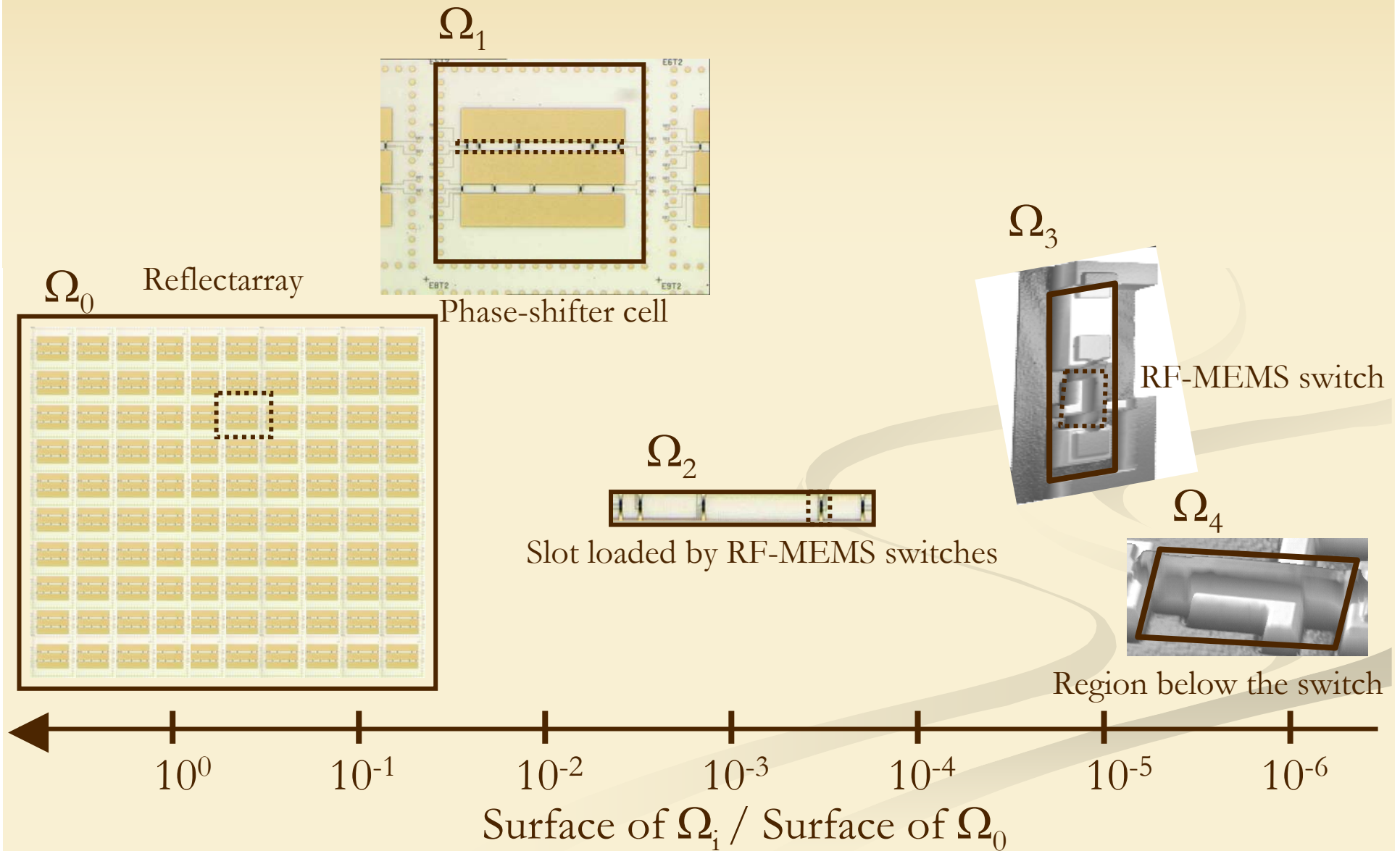
(*) Cadoret D., Laisne A., Gillard R. and Legay H., *Microwave and Optical Technological Letters* (2005)



Top view

**$2^{10} = 1024$ ON/OFF states configurations for achieving the
phase-shift range of 360°**

Visualization of the multiple scale levels



Typical numerical problems when modeling multi-scale structures

→ Classical meshing-based techniques :

- ✓ Ill-conditioned matrices
- ✓ Numerical convergence problem and/or very time-consuming



→ Hybrid techniques (Global modeling) :

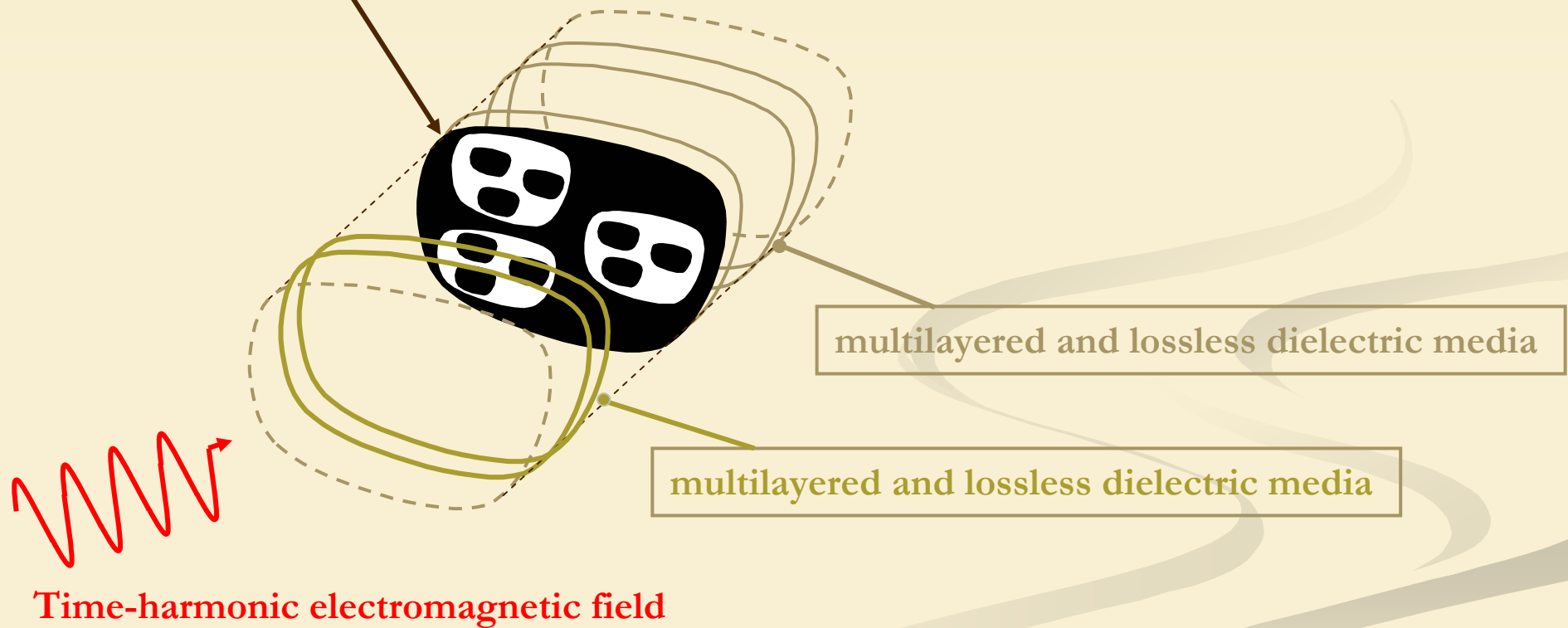
- ✓ Connections may be delicate from a theoretical and practical points of view

Need for new theoretical approaches for the modeling and design of multi-scale structures

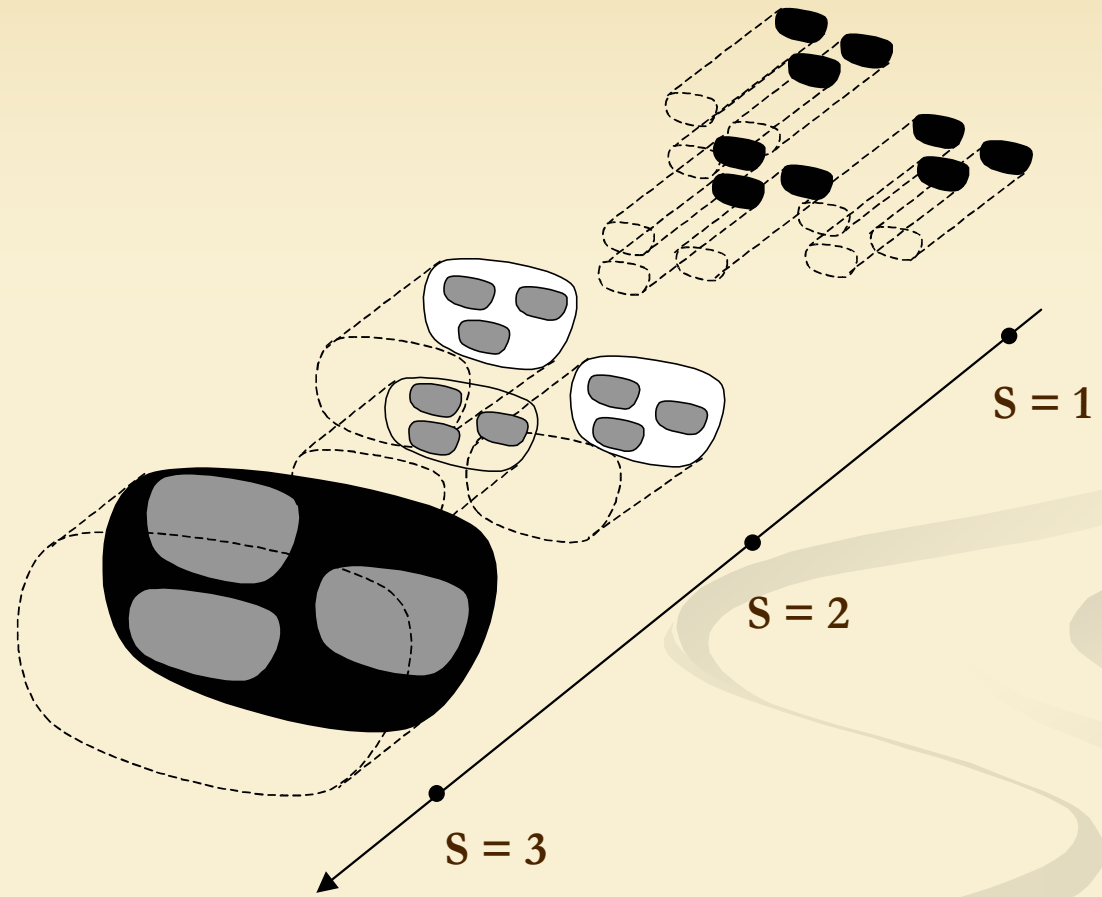
→ Scale Changing Technique (SCT) : monolithic (unique) formulation

Scale Changing Technique (SCT)

Discontinuity plane :  *Perfect Electric Conductor*
 *Dielectric interface*



1. partitioning process

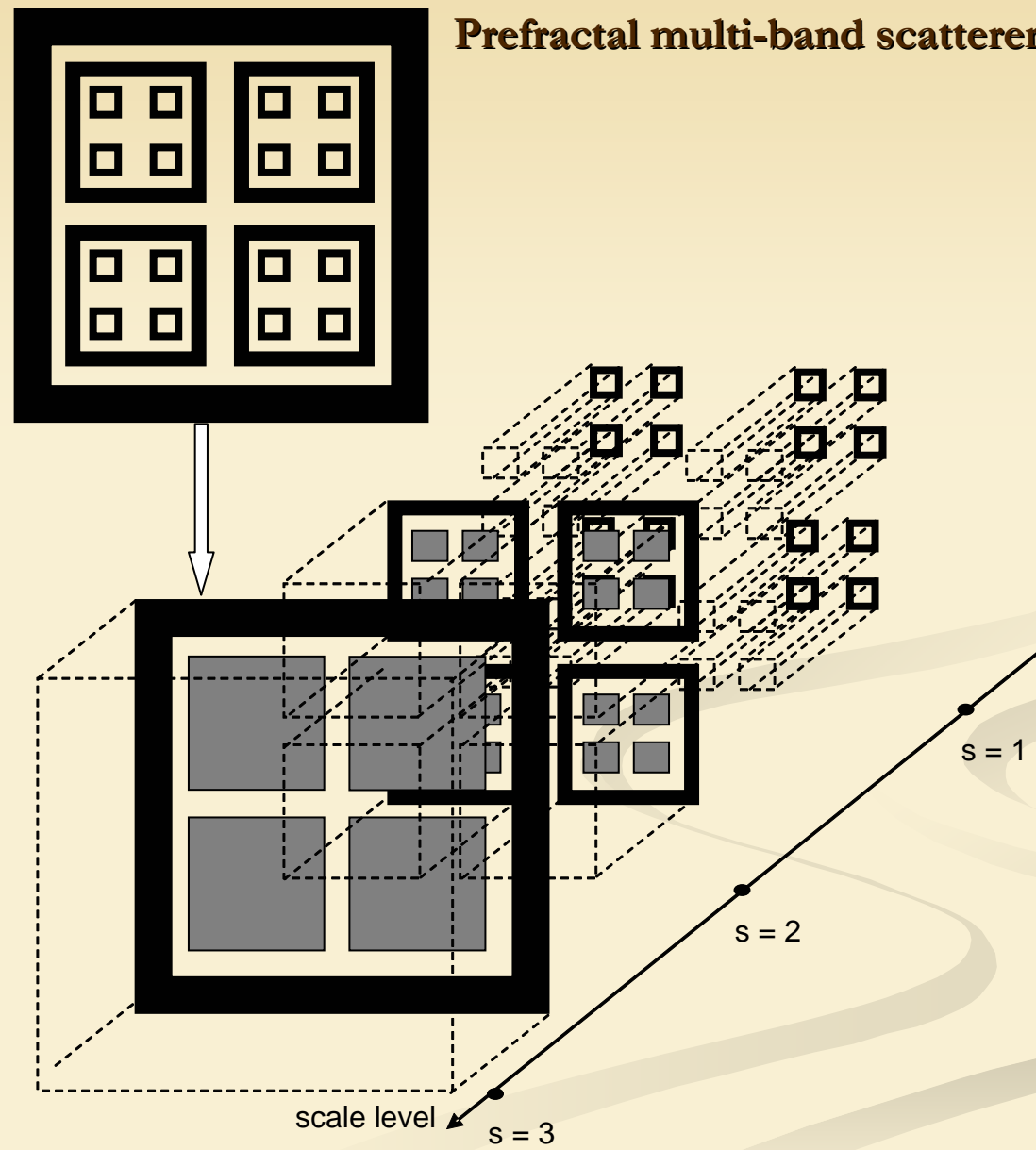


Scale level s

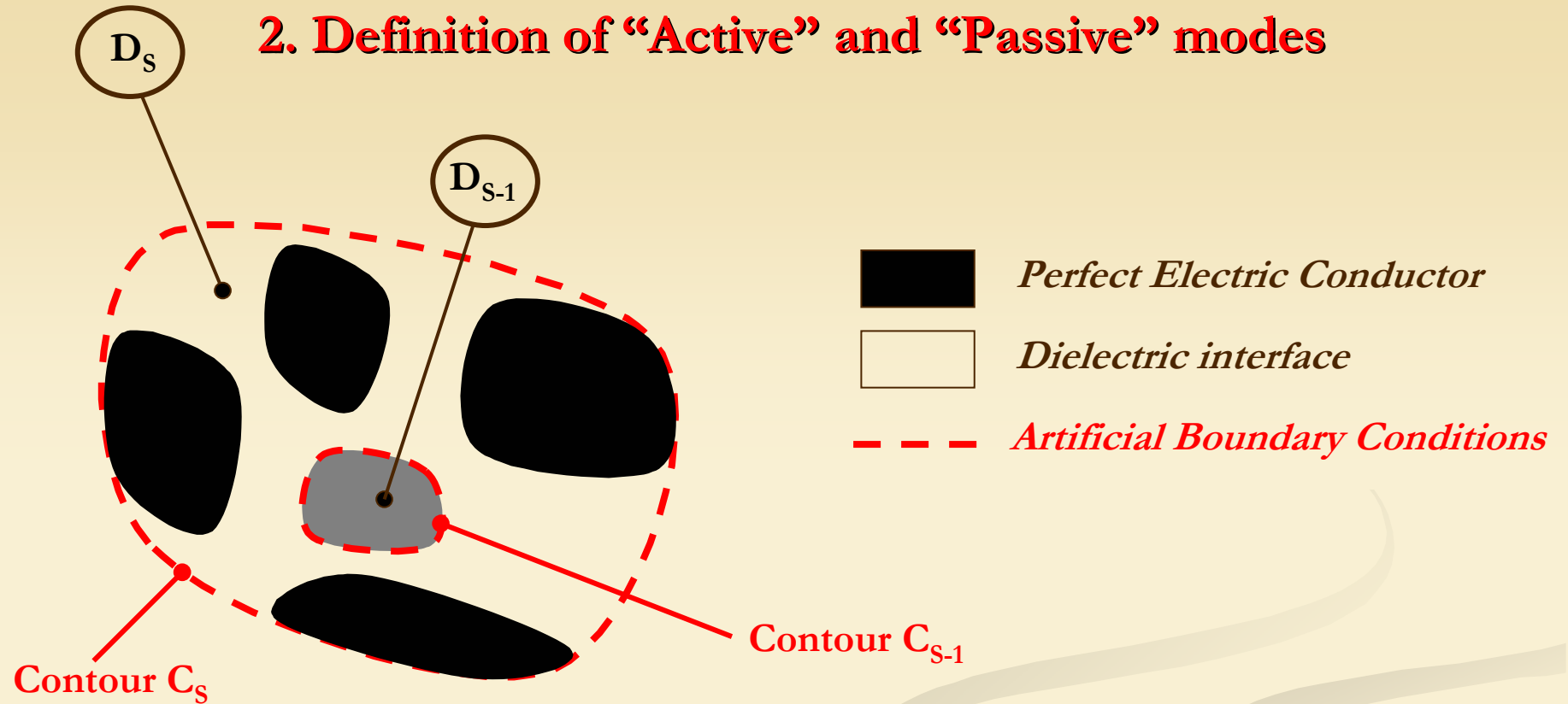
hierarchical domain-decomposition

Example :

Prefractal multi-band scatterer



2. Definition of “Active” and “Passive” modes



→ Derivation of the *modal basis* in D_S and D_{S-1} :

$$\begin{cases} \left[\nabla_T^2 + k_n^{(s)2} \right] \vec{F}_n^{(s)} = \vec{0} \\ \text{B.C. along } C_S \end{cases}$$

and

$$\begin{cases} \left[\nabla_T^2 + k_n^{(s-1)2} \right] \vec{F}_n^{(s-1)} = \vec{0} \\ \text{B.C. along } C_{S-1} \end{cases}$$

Tangential electric field in D_s : **smooth variations** & highly irregular fluctuations

$$\vec{E}^{(s)} = \sum_{n=1}^{\infty} V_n^{(s)} \vec{F}_n^{(s)} = \boxed{\sum_{n=1}^{N^{(s)}} V_n^{(s)} \vec{F}_n^{(s)}} + \boxed{\sum_{N^{(s)}+1}^{\infty} V_n^{(s)} \vec{F}_n^{(s)}}$$

Large-scale (spectrally localized)

Linear combination of few
lower-order modes in D_s

Participate in the description of the
coupling between smaller
sub-domains in D_s

« Active » modes

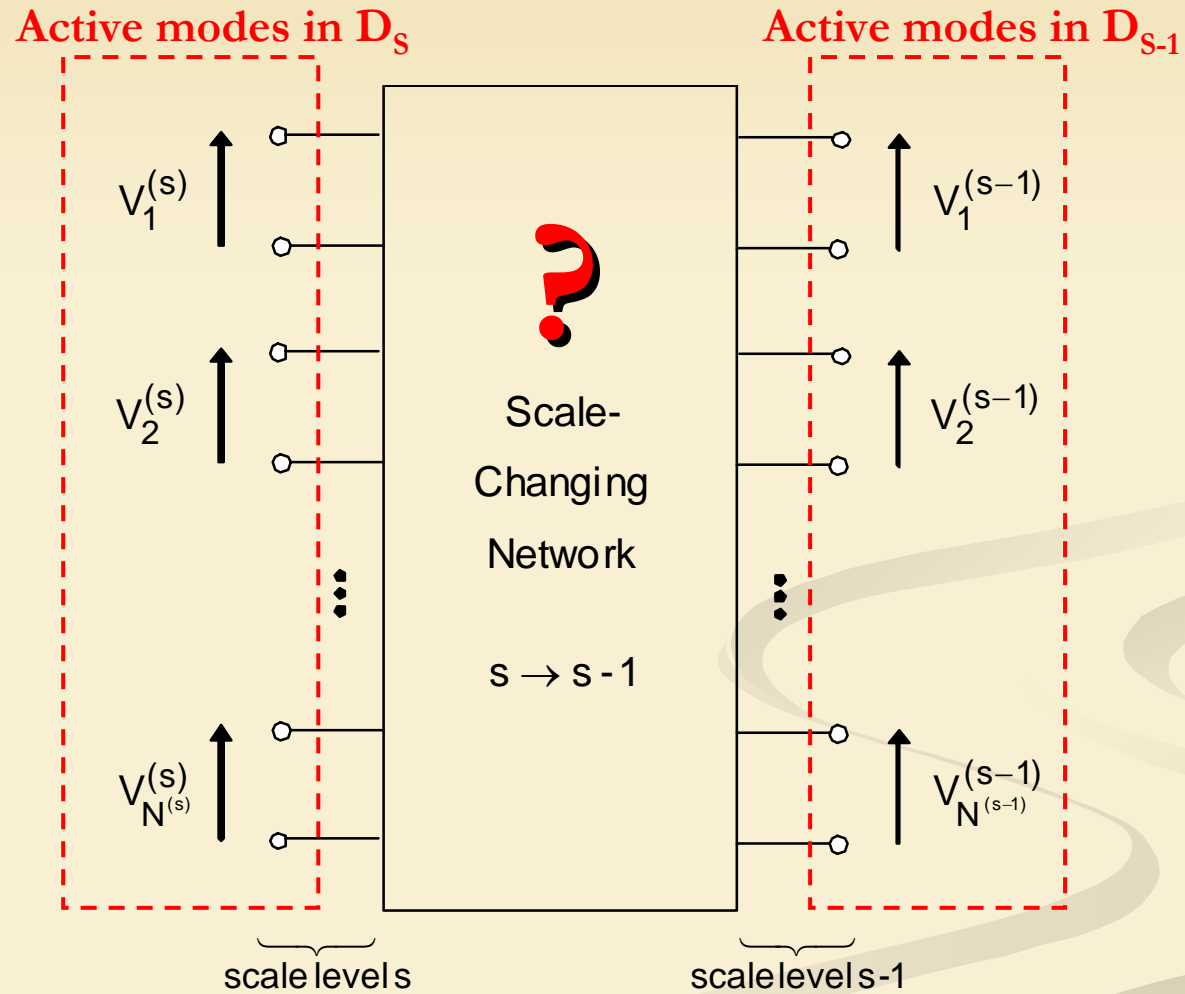
Fine-scale (spatially localized)

Linear combination of an
infinite number of
higher-order modes in D_s

Contributes significantly to the
representation of the field only
in the vicinity of discontinuities
and sharp edges

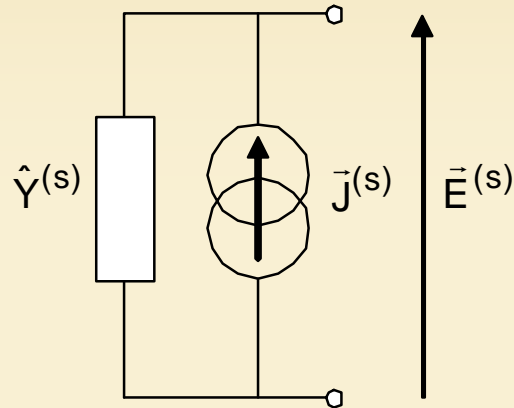
« Passive » modes

3. Derivation of the “Scale-Changing Network” *



→ **Active modes** in D_s and D_{s-1} are taken as **field excitations**:

- “Scale-Changing Sources” at the large scale D_s



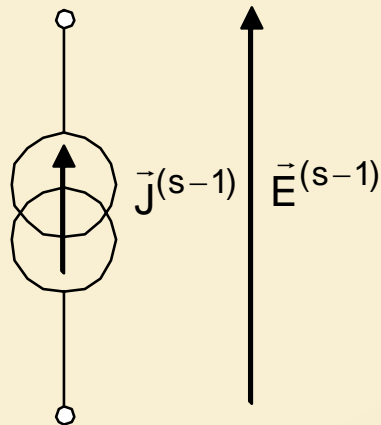
$$\vec{J}^{(s)} = \sum_{n=1}^{N^{(s)}} I_n^{(s)} \vec{F}_n^{(s)}$$

Known combination of active modes

$$\hat{Y}^{(s)} = \sum_{n=N^{(s)}+1}^{\infty} \left| \vec{F}_n^{(s)} \right\rangle Y_n^{(s)} \left\langle \vec{F}_n^{(s)} \right|$$

Passive mode are shunted by their modal admittance

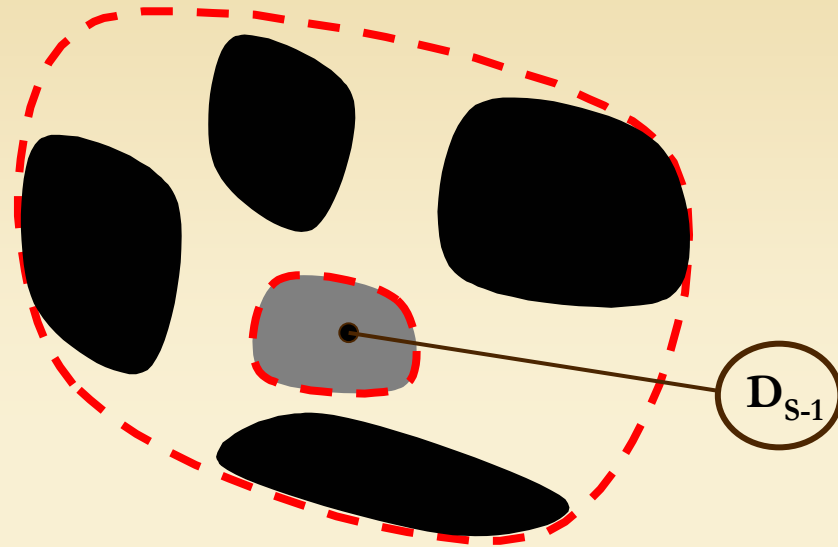
- “Scale-Changing Sources” at the smaller scale D_{s-1}



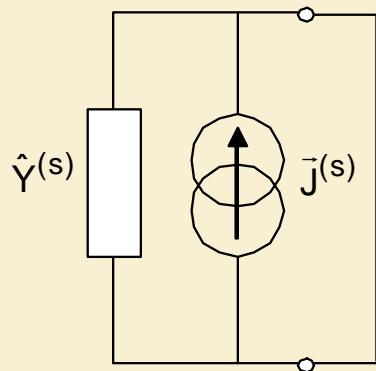
$$\vec{J}^{(s-1)} = \sum_{n=1}^{N^{(s-1)}} I_n^{(s-1)} \vec{F}_n^{(s-1)}$$

Known combination of active modes

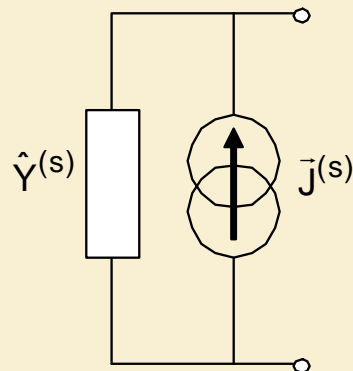
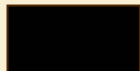
→ Formulation of the **boundary value problem** in D_S



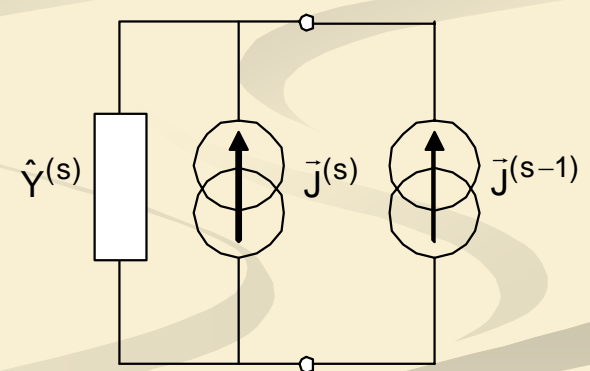
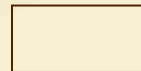
● *Equivalent circuits that model the boundary conditions :*



in the perfect electric
conductors domain



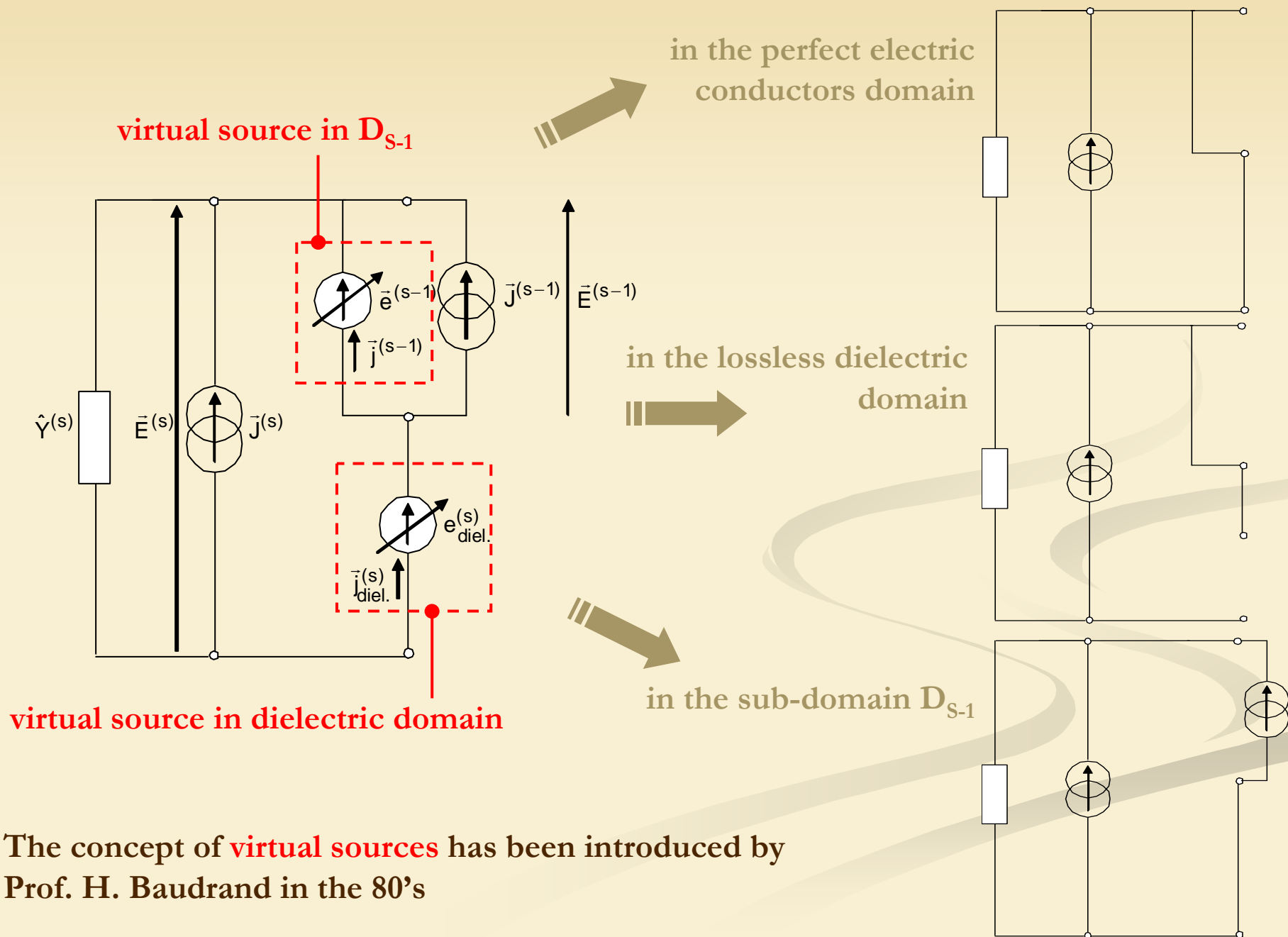
in the lossless
dielectric domain



in the sub-domain D_{S-1}



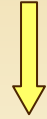
● *Equivalent network representation of B.C. in the domain D_S*



The concept of **virtual sources** has been introduced by Prof. H. Baudrand in the 80's

● *Derivation of the boundary value problem*

Kirchhoff's and Ohm's laws applied to the equivalent network :



$$\underbrace{\begin{bmatrix} \vec{E}^{(s)} \\ \vec{E}^{(s-1)} \\ \vec{j}^{(s-1)} \\ j_{\text{diel}}^{(s)} \end{bmatrix}}_{\text{dual quantities of the sources}} = \begin{bmatrix} 0 & 0 & \hat{1} & \hat{1} \\ 0 & 0 & \hat{1} & 0 \\ -\hat{1} & -\hat{1} & \hat{Y}^{(s)} & \hat{Y}^{(s)} \\ -\hat{1} & 0 & \hat{Y}^{(s)} & \hat{Y}^{(s)} \end{bmatrix} \underbrace{\begin{bmatrix} \vec{j}^{(s)} \\ \vec{j}^{(s-1)} \\ \vec{e}^{(s-1)} \\ \vec{e}_{\text{diel}}^{(s)} \end{bmatrix}}_{\text{sources}}$$

with $\vec{e}^{(s-1)}$ and $\vec{e}_{\text{diel}}^{(s)}$ virtual sources, i.e.:

$$\begin{cases} \vec{j}^{(s-1)} = \vec{0} & \text{in sub-domain } D^{(s-1)} \\ j_{\text{diel}}^{(s)} = \vec{0} & \text{in the dielectric domain} \end{cases}$$

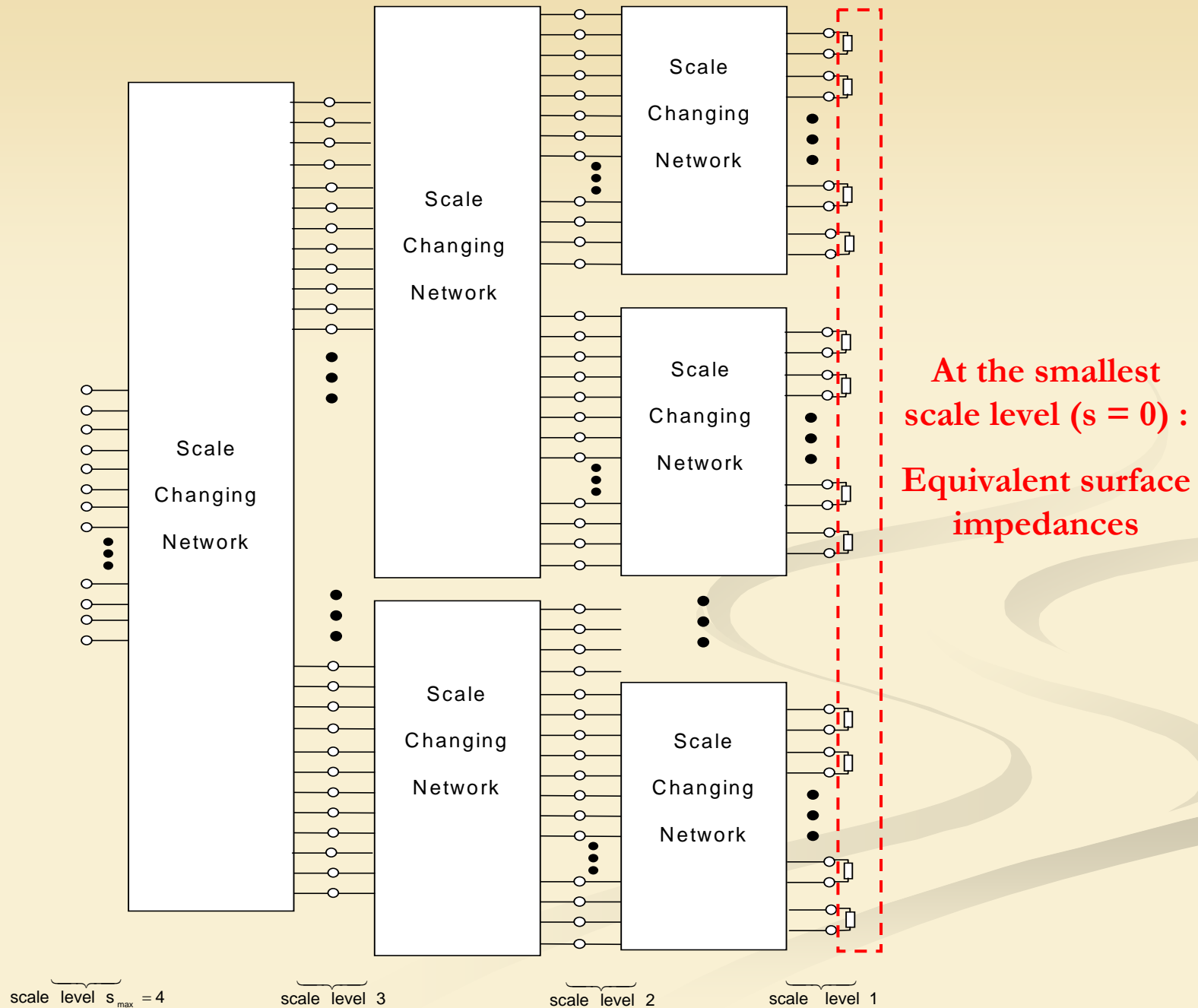
● *Numerical resolution by applying Galerkin's method*

Choice of two sets of entire-domain trial functions for the expansion of the two (unknown) virtual sources :

$$\begin{bmatrix} \begin{bmatrix} V^{(s)} \\ V^{(s-1)} \\ 0 \\ 0 \end{bmatrix} \end{bmatrix} = \begin{bmatrix} \begin{bmatrix} 0 \\ 0 \\ -P \\ -Q \end{bmatrix}^{*T} \\ \begin{bmatrix} 0 \\ 0 \\ -R \\ 0 \end{bmatrix}^{*T} \\ \begin{bmatrix} P \\ R \\ \hat{Y} \\ \hat{Y} \end{bmatrix}_{21} \\ \begin{bmatrix} Q \\ 0 \\ \hat{Y} \\ \hat{Y} \end{bmatrix}_{22} \end{bmatrix} \begin{bmatrix} \begin{bmatrix} I^{(s)} \\ I^{(s-1)} \\ a^{(s-1)} \\ a^{(s)} \end{bmatrix} \end{bmatrix}$$

$$\begin{bmatrix} \begin{bmatrix} V^{(s)} \\ V^{(s-1)} \end{bmatrix} \end{bmatrix} = \begin{bmatrix} \Sigma^{(s,s-1)} \end{bmatrix} \begin{bmatrix} \begin{bmatrix} I^{(s)} \\ I^{(s-1)} \end{bmatrix} \end{bmatrix}$$

3. Global EM Simulation by cascading SCNs



Key advantages of the Scale Changing Technique

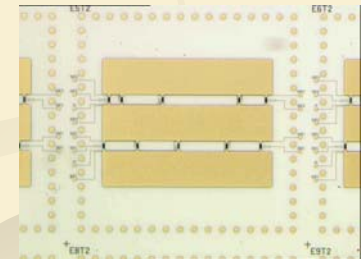
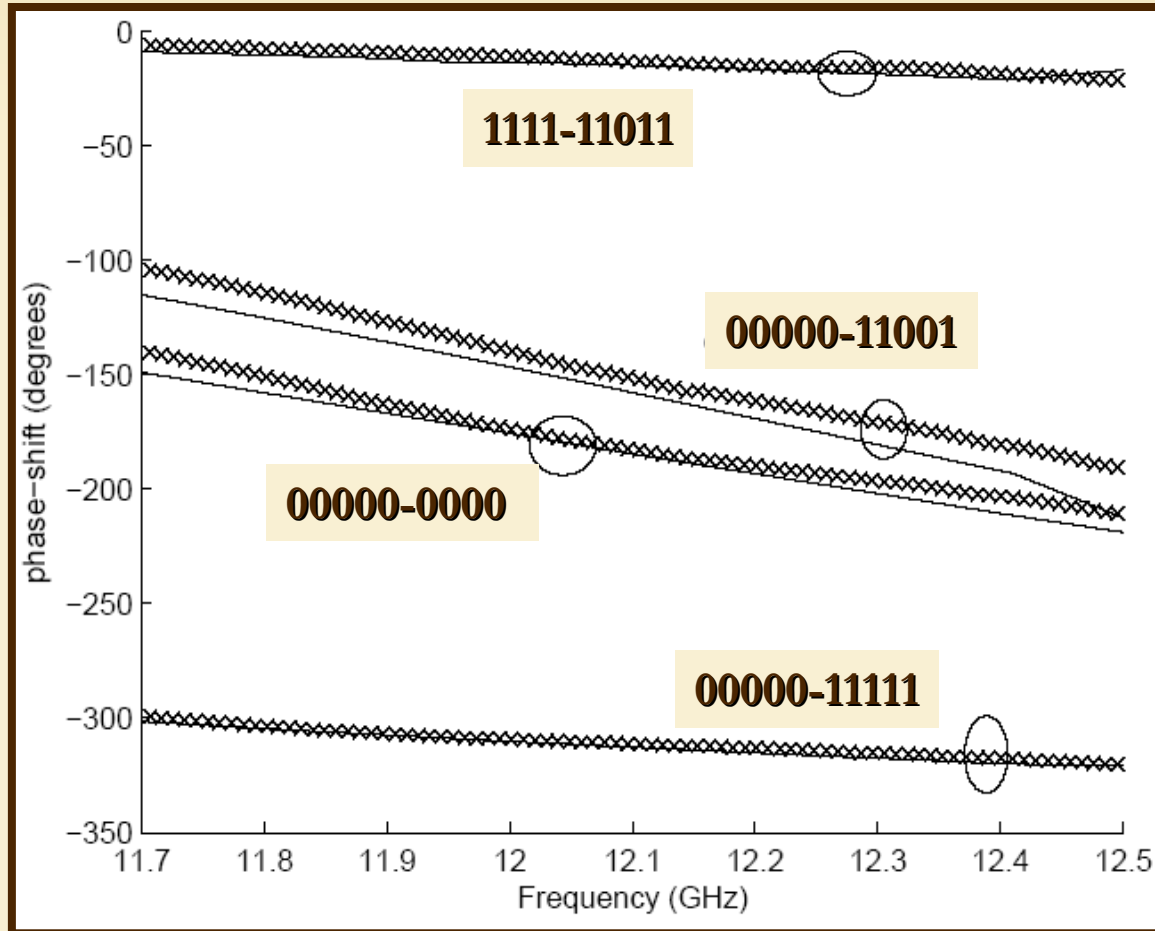
- ✓ Judicious partitioning of the discontinuity plane avoids critical aspect ratios
- ✓ Fine description of the electromagnetic field at each scale may be reached
- ✓ Modifications of the geometry at a given scale does not require the recalculation of the overall structure (modular approach)
- ✓ Scale changing networks are computed separately : highly parallelizable

Difficulties

- ✓ Systematic convergence studies on the number of modes are required
- ✓ No systematic rules for the choice of the boundary conditions

Example No1 : MEMS-controlled planar Phase-shifter *

- (—) Experimental data (waveguide simulator technique)
- (xxxx) Scale-Changing Technique



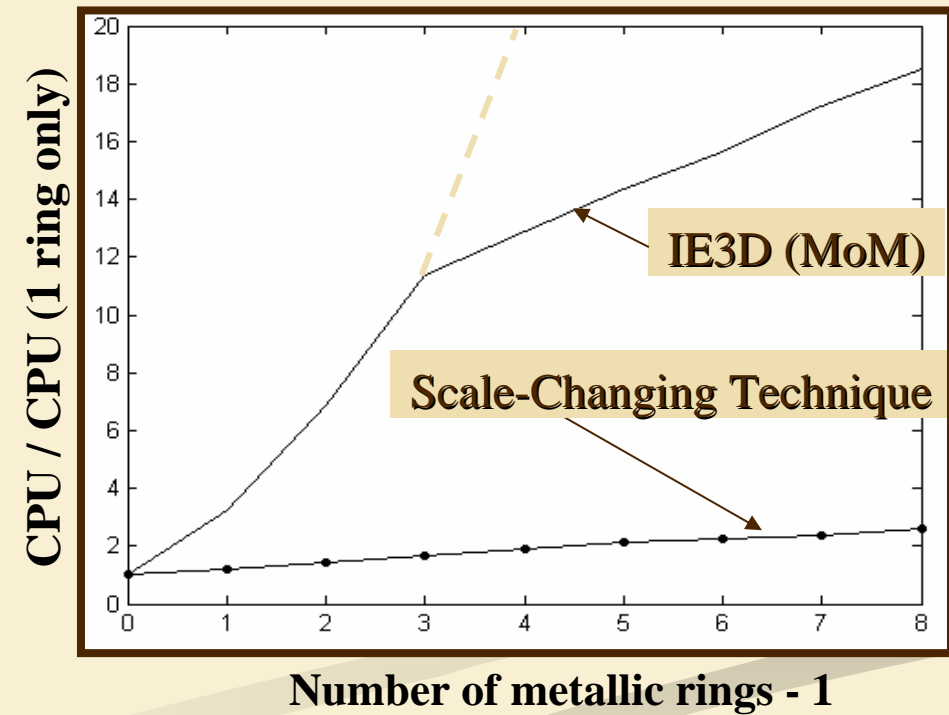
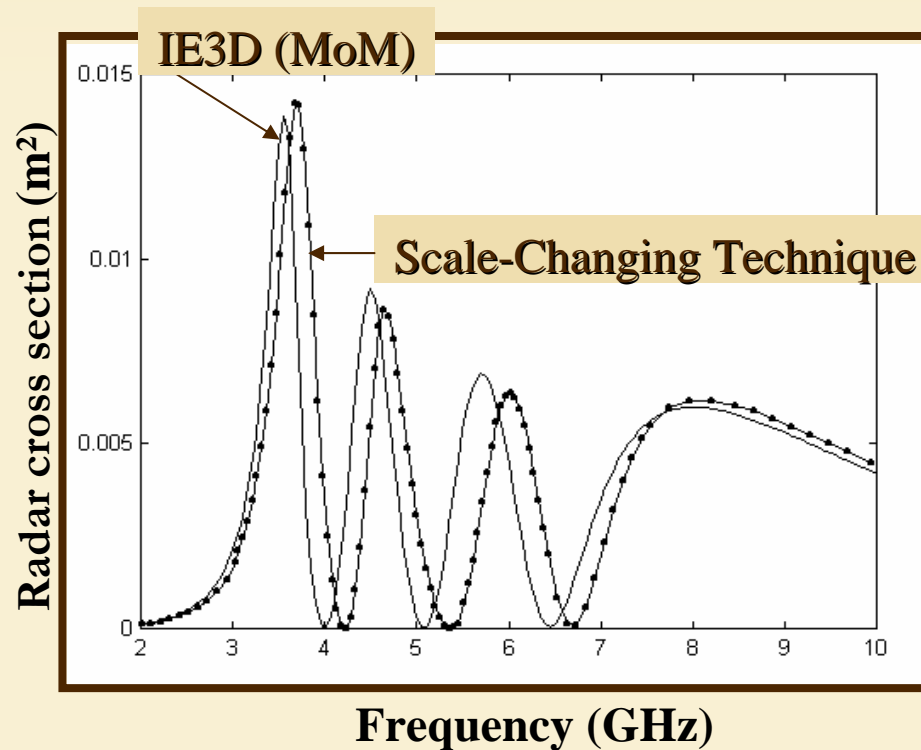
0 : switch is OFF
1 : switch is ON

* From E. Perret, H. Aubert, H. Legay, *IEEE Trans. On Microwave Theory and Tech.* (2006)

Example No2 : Multi-band scatterer *

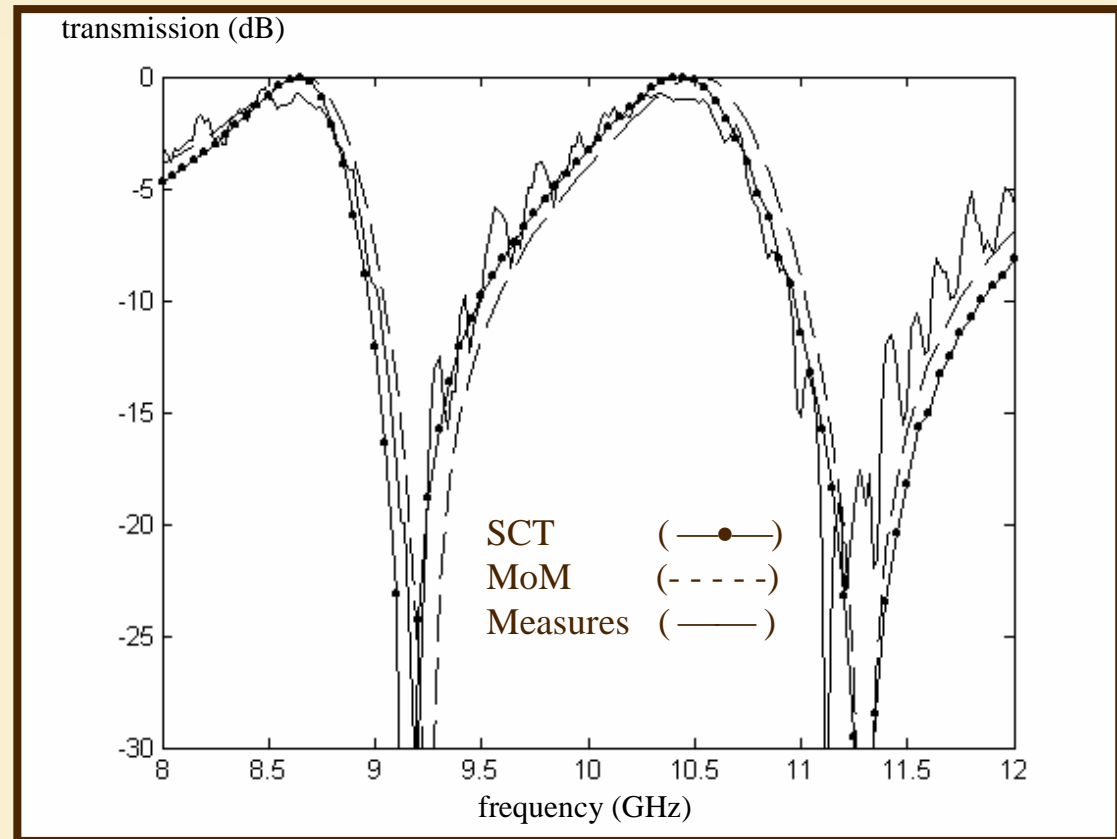
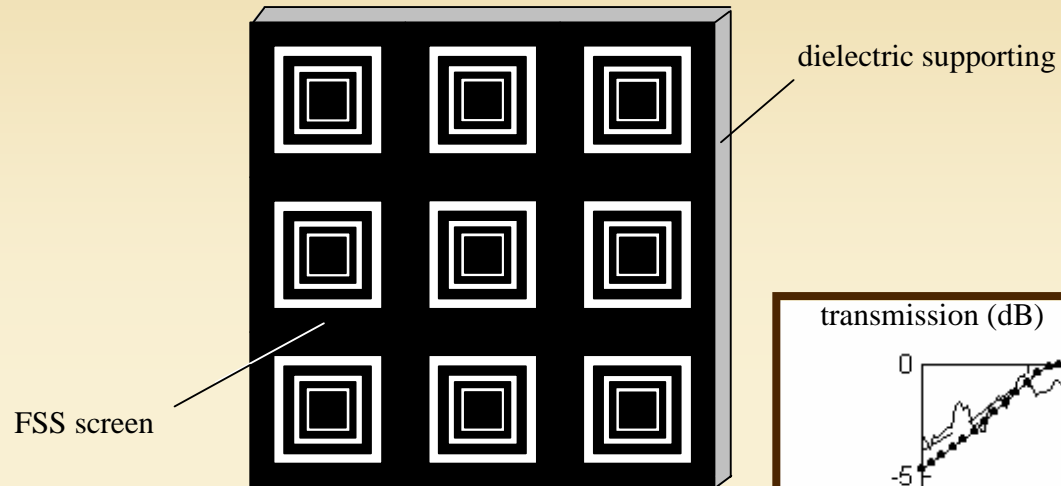


Concentric metallic rings



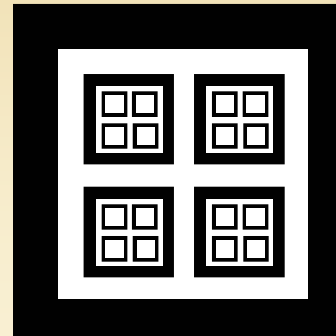
* From D. Voyer, H. Aubert, J. David, *Electronics Letters*, Feb. 2005

Exemple No3 : Multi-Frequency Selective Surface *



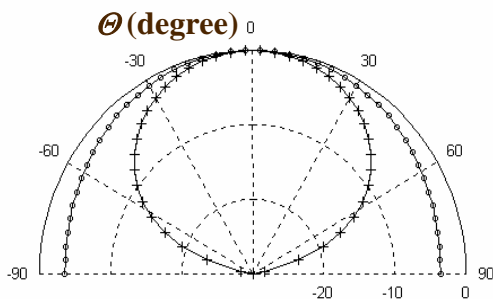
* From D. Voyer, H. Aubert, J. David, *IEEE Trans. Antennas Propagat.* (Oct. 2006)

Example No4 : Finite-size multi-frequency selective surface *



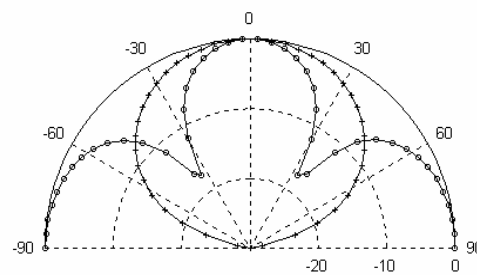
Sierpinski carpet

(a) 3.7GHz

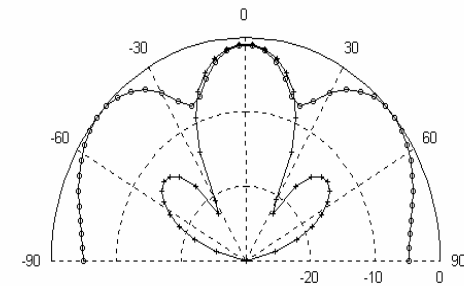


Normalized scattered field (dB)

(b) 11GHz



(c) 17.9GHz



+ IE3D (MoM)

— Scale-Changing Technique

* From D. Voyer, H. Aubert, J. David, *IEEE Trans. Antennas Propagat.* (Oct. 2006)

The applications of SCT for the electromagnetic simulation of ...

1. Active antennas in non linear regime

*Hybridization of SCT with the Multi-domain approach
in collaboration with ONERA, PhD. Studies funded by Thalès (2005-2008)*

2. Reflectarrays with coupled disassemblable cells

PhD. Studies funded by Thalès/ Midi-Pyrénées Regional Council (2006-2009)

3. Very Large Structures

BQR PRES Toulouse in collaboration with IRIT (2009)

4. Multi-scale structures

*Implementation of SCT in Grid Computing environment
ANR Project : Multi-scale modeling: from Electromagnetism to the GRID
in collaboration with ID Lab. Grenoble (2007-2010)*

5. Periodical Frequency Selective surfaces

PhD. Studies funded by CNES (2007-2010)

The future of the Scale-Changing Technique (SCT)

1. Hybridization of SCT with full-wave 3D techniques
(TLM, Multi-domain approach)

Complex structures 3D

2. Implementation of SCT in Grid Computing environment

“Scale-driven” scheduler